

Solutions

3.1	The pressure is given by the hydrostatic pressure $p(x, z) = \rho_{\text{ice}} g (H(x) - z)$, which is zero at the surface.	0.3
3.2a	<p>The outward force on a vertical slice at a distance x from the middle and of a given width Δy is obtained by integrating up the pressure times the area:</p> $F(x) = \Delta y \int_0^{H(x)} \rho_{\text{ice}} g (H(x) - z) dz = \frac{1}{2} \Delta y \rho_{\text{ice}} g H(x)^2$ <p>which implies that $\Delta F = F(x) - F(x + \Delta x) = -\frac{dF}{dx} \Delta x = -\Delta y \rho_{\text{ice}} g H(x) \frac{dH}{dx} \Delta x$. This finally shows that</p> $S_b = \frac{\Delta F}{\Delta x \Delta y} = -\rho_{\text{ice}} g H(x) \frac{dH}{dx}$ <p>Notice the sign, which must be like this, since S_b was defined as positive and $H(x)$ is a decreasing function of x.</p>	0.9
3.2b	<p>To find the height profile, we solve the differential equation for $H(x)$:</p> $-\frac{S_b}{\rho_{\text{ice}} g} = H(x) \frac{dH}{dx} = \frac{1}{2} \frac{d}{dx} H(x)^2$ <p>with the boundary condition that $H(L) = 0$. This gives the solution:</p> $H(x) = \sqrt{\frac{2S_b L}{\rho_{\text{ice}} g}} \sqrt{1 - x/L}$ <p>Which gives the maximum height $H_m = \sqrt{\frac{2S_b L}{\rho_{\text{ice}} g}}$.</p> <p>Alternatively, dimensional analysis could be used in the following manner. First notice that $\mathcal{L} = [H_m] = [\rho_{\text{ice}}^\alpha g^\beta \tau_b^\gamma L^\delta]$. Using that $[\rho_{\text{ice}}] = \mathcal{M} \mathcal{L}^{-3}$, $[g] = \mathcal{L} \mathcal{T}^{-2}$, $[\tau_b] = \mathcal{M} \mathcal{L}^{-1} \mathcal{T}^{-2}$, demands that $\mathcal{L} = [H_m] = [\rho_{\text{ice}}^\alpha g^\beta \tau_b^\gamma L^\delta] = \mathcal{M}^{\alpha+\gamma} \mathcal{L}^{-3\alpha+\beta-\gamma+\delta} \mathcal{T}^{-2\beta-2\gamma}$, which again implies $\alpha + \gamma = 0$, $-3\alpha + \beta - \gamma + \delta = 1$, $2\beta + 2\gamma = 0$. These three equations are solved to give $\alpha = \beta = -\gamma = \delta - 1$, which shows that</p> $H_m \propto \left(\frac{S_b}{\rho_{\text{ice}} g} \right)^\gamma L^{1-\gamma}$ <p>Since we were informed that $H_m \propto \sqrt{L}$, it follows that $\gamma = 1/2$. With the boundary condition $H(L) = 0$, the solution then take the form</p> $H(x) \propto \left(\frac{S_b}{\rho_{\text{ice}} g} \right)^{1/2} \sqrt{L - x}$ <p>The proportionality constant of $\sqrt{2}$ cannot be determined in this approach.</p>	0.8

3.2c	<p>For the rectangular Greenland model, the area is equal to $A = 10L^2$ and the volume is found by integrating up the height profile found in problem 3.2b:</p> $V_{G,ice} = (5L)2 \int_0^L H(x) dx = 10L \int_0^L \left(\frac{\tau_b L}{\rho_{ice} g}\right)^{1/2} \sqrt{1 - x/L} dx = 10H_m L^2 \int_0^1 \sqrt{1 - \tilde{x}} d\tilde{x}$ $= 10H_m L^2 \left[-\frac{2}{3}(1 - \tilde{x})^{3/2}\right]_0^1 = \frac{20}{3} H_m L^2 \propto L^{5/2},$ <p>where the last line follows from the fact that $H_m \propto \sqrt{L}$. Note that the integral need not be carried out to find the scaling with L. This implies that $V_{G,ice} \propto A_G^{5/4}$ and the wanted exponent is $\gamma = 5/4$.</p>	0.5
3.3	<p>According to the assumption of constant accumulation c the total mass accumulation rate from an area of width Δy between the ice divide at $x = 0$ and some point at $x > 0$ must equal the total mass flux through the corresponding vertical cross section at x. That is: $\rho c x \Delta y = \rho \Delta y H_m v_x(x)$, from which the velocity is isolated:</p> $v_x(x) = \frac{cx}{H_m}$	0.6
3.4	<p>From the given relation of incompressibility it follows that</p> $\frac{dv_z}{dz} = -\frac{dv_x}{dx} = -\frac{c}{H_m}$ <p>Solving this differential equation with the initial condition $v_z(0) = 0$, shows that:</p> $v_z(z) = -\frac{cz}{H_m}$	0.6
3.5	<p>Solving the two differential equations</p> $\frac{dz}{dt} = -\frac{cz}{H_m} \quad \text{and} \quad \frac{dx}{dt} = \frac{cx}{H_m}$ <p>with the initial conditions that $z(0) = H_m$, and $x(0) = x_i$ gives</p> $z(t) = H_m e^{-ct/H_m} \quad \text{and} \quad x(t) = x_i e^{ct/H_m}$ <p>This shows that $z = H_m x_i / x$, meaning that flow lines are hyperbolas in the xz-plane. Rather than solving the differential equations, one can also use them to show that</p> $\frac{d}{dt}(xz) = \frac{dx}{dt}z + x\frac{dz}{dt} = \frac{cx}{H_m}z - x\frac{cz}{H_m} = 0$ <p>which again implies that $xz = \text{const}$. Fixing the constant by the initial conditions, again leads to the result that $z = H_m x_i / x$.</p>	0.9
3.6	<p>At the ice divide, $x = 0$, the flow will be completely vertical, and the t-dependence of z found in 3.5 can be inverted to find $\tau(z)$. One finds that $\tau(z) = \frac{H_m}{c} \ln\left(\frac{H_m}{z}\right)$.</p>	1.0

3.7a	<p>The present interglacial period extends to a depth of 1492 m, corresponding to 11,700 year. Using the formula for $\tau(z)$ from problem 3.6, one finds the following accumulation rate for the interglacial:</p> $c_{ig} = \frac{H_m}{11,700 \text{ years}} \ln \left(\frac{H_m}{H_m - 1492 \text{ m}} \right) = 0.1749 \text{ m/year.}$ <p>The beginning of the ice age 120,000 years ago is identified as the drop in $\delta^{18}\text{O}$ in figure 3.2b at a depth of 3040 m. Using the vertical flow velocity found in problem 3.4, one has $\frac{dz}{z} = -\frac{c}{H_m} dt$, which can be integrated down to a depth of 3040 m, using a stepwise constant accumulation rate:</p> $\begin{aligned} H_m \ln \left(\frac{H_m}{H_m - 3040 \text{ m}} \right) &= -H_m \int_{H_m}^{H_m - 3040 \text{ m}} \frac{1}{z} dz \\ &= \int_{11,700 \text{ year}}^{120,000 \text{ year}} c_{ia} dt + \int_0^{11,700 \text{ year}} c_{ig} dt \\ &= c_{ia}(120,000 \text{ year} - 11,700 \text{ year}) + c_{ig} 11,700 \text{ year} \end{aligned}$ <p>Isolating form this equation leads to $c_{ia} = 0.1232$, i.e. far less precipitation than now.</p>	0.8
3.7b	<p>Reading off from figure 3.2b: $\delta^{18}\text{O}$ changes from $-43,5 \text{ ‰}$ to $-34,5 \text{ ‰}$. Reading off from figure 3.2a, T then changes from -40 °C to -28 °C. This gives $\Delta T \approx 12 \text{ °C}$.</p>	0.2
3.8	<p>From the area A_G one finds that $L = \sqrt{A_G/10} = 4.14 \times 10^5 \text{ m}$. Inserting numbers in the volume formula found in 3.2c, one finds that:</p> $V_{G,ice} = \frac{20}{3} L^{5/2} \sqrt{\frac{2S_b}{\rho_{ice}g}} = 3.45 \times 10^{15} \text{ m}^3$ <p>This ice volume must be converted to liquid water volume, by equating the total masses, i.e. $V_{G,wa} = V_{G,ice} \frac{\rho_{ice}}{\rho_{wa}} = 3.17 \times 10^{15} \text{ m}^3$, which is finally converted to a sea level rise, as $h_{G,rise} = \frac{V_{G,wa}}{A_o} = 8.79 \text{ m}$.</p>	0.6

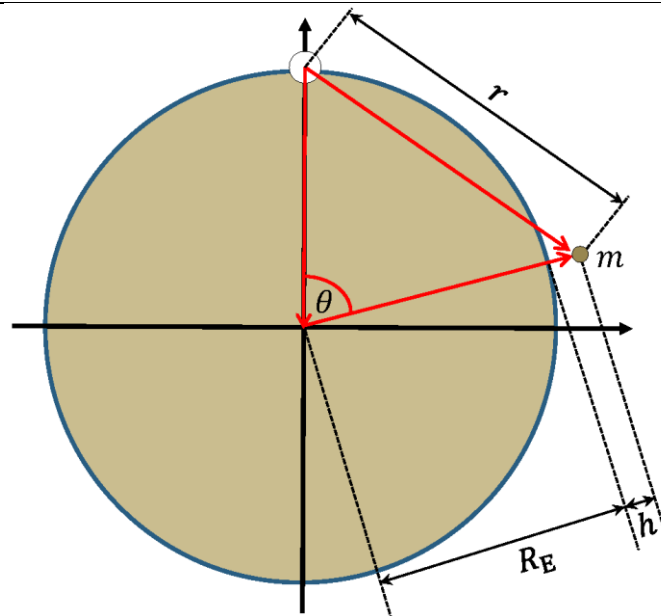


Figure 3.S1 Geometry of the ice ball (white circle) with a test mass m (small gray circle).

The total mass of the ice is

$$M_{\text{ice}} = V_{G,\text{ice}} \rho_{\text{ice}} = 3.17 \times 10^{18} \text{ kg} = 5.31 \times 10^{-7} m_E$$

- 3.9 The total gravitational potential felt by a test mass m at a certain height h above the surface of the Earth, and at a polar angle θ (cf. figure 3.S1), with respect to a rotated polar axis going straight through the ice sphere is found by adding that from the Earth with that from the ice:

1.6

$$U_{\text{tot}} = -\frac{Gm_E m}{R_E + h} - \frac{GM_{\text{ice}} m}{r} = -mgR_E \left(\frac{1}{1 + h/R_E} + \frac{M_{\text{ice}}/m_E}{r/R_E} \right)$$

where $g = Gm_E/R_E^2$. Since $h/R_E \ll 1$ one may use the approximation given in the problem, $(1 + x)^{-1} \approx 1 - x$, $|x| \ll 1$, to approximate this by

$$U_{\text{tot}} \approx -mgR_E \left(1 - \frac{h}{R_E} + \frac{M_{\text{ice}}/m_E}{r/R_E} \right).$$

Isolating h now shows that $h = h_0 + \frac{M_{\text{ice}}/m_E}{r/R_E} R_E$, where $h_0 = R_E + U_{\text{tot}}/(mg)$. Using again that $h/R_E \ll 1$, trigonometry shows that $r \approx 2R_E |\sin(\theta/2)|$, and one has:

$$h(\theta) - h_0 \approx \frac{M_{\text{ice}}/m_E}{2|\sin(\theta/2)|} R_E \approx \frac{1.69 \text{ m}}{|\sin(\theta/2)|}$$

To find the magnitude of the effect in Copenhagen, the distance of 3500 km along the surface is used to find the angle $\theta_{\text{CPH}} = (3.5 \times 10^6 \text{ m})/R_E \approx 0.549$, corresponding to $h_{\text{CPH}} - h_0 \approx 6.25 \text{ m}$. Directly opposite to Greenland corresponds to $\theta = \pi$, which gives $h_{\text{OPP}} - h_0 \approx 1.69 \text{ m}$. The difference is then $h_{\text{CPH}} - h_{\text{OPP}} \approx 4.56 \text{ m}$, where h_0 has dropped out.

Total

9.0